

# The computer modeling of the physical mechanism of the 2D convective transport of hydrocarbons from the mantle wedge to the Earth's surface: a comparison of the Newtonian and non-Newtonian rheology cases

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**Abstract**— For the non-Newtonian mantle rheology case the 2D thermal viscous dissipation-driven thermal convection in the mantle wedge above the Apulian lithospheric microplate subducting under the Euro-Asian plate is modeled numerically. The effects of the 410 km and 660 km phase transitions are taken into account. Within the framework of the model constructed the horizontal extent of the 2D heat flux anomaly observed in the rear of the Dinarides mountain belt corresponds to subduction velocity of  $\sim 10$  mm per year which is close to that observed with the help of geodetic means. In the case of non-Newtonian rheology the upwelling convective flow transporting heat to the Earth's surface locates at the distance from the trench corresponding to the actually observed 2D heat flux anomaly, the velocity in the convective vortices being from  $\sim 10$  mm per year to  $\sim 10$  m per year for the water content in the mantle wedge from  $0.3 \times 10^{-1}$  to  $3 \times 10^{-1}$  weight percent respectively. The convection cell dimension is of the order of the horizontal scale of the heat flux anomaly observed in the Pannonia petroleum basin and Vardar zone. Upwelling mantle wedge convective flow is indicated to be able to provide the mantle wedge hydrocarbons transport to the Earth's surface for the mantle wedge mantle content over  $0.3 \times 10^{-1}$  weight percent.

**Keywords**— Computer Modeling, Thermal Convection, Newtonian & Non-Newtonian Rheology Cases.

## I. INTRODUCTION

According to [3], the subduction of the Apulian lithospheric microplate under the Dinarides, Pannonia basin and Vardar zone is sufficiently flat and during the last  $\sim 45$  Ma occurred at the angle of  $\sim 25^\circ$ , which remained unchanged during this time interval. The genesis of the Dinarides mountain belt (with the transversal horizontal extent of  $\sim 300$  km) apparently is of the thrust and fold nature, associated with the former collision and subduction of the oceanic branches of the Neo-Tethys and Alpine-Tethys as the result of thrusting of the African plate under the Eastern and Western Europe during the last 55 – 35 Ma [3]. In [1] numerous papers are referred, containing contradictory estimates of the relative motions of the Apulian lithospheric microplate and Euro-Asian plates, made on the basis of seismic, geophysical and geodetic data. In fig. 3 in [Op. cit.] the velocity of subduction of the Apulian lithospheric microplate under the Euro-Asian one is seen to amount to  $\sim 5 - 8$  mm $\times$ a<sup>-1</sup> according to referred works, while in [1] this velocity is estimated to be of the order of  $\sim 5$  mm $\times$ a<sup>-1</sup> according to calculations based on geodetic observations. In [12] the Pannonia petroleum basin and Vardar zone are noted to be the zones of the Middle Miocene extension occurred  $\sim 14 - 11.6$  Ma ago, which led to the lithosphere thinning, these zones being the back-arc basin characterized by the back-arc spreading. At that time the single mountain belt parallel to Apulian shore was split into Carpathians and Dinarides and the shallow Pannonian sea was formed, which existed approximately to 600 thousand years ago. Presently the Pannonian oil- and gas-bearing basin is situated in this region. Here the conditions are clarified under which the centre of the back-arc spreading initiates as the result of convective instability, driven by the dissipative heat release in the mantle wedge above the subducting Apulian lithospheric microplate.

According to [4, 8, 9] two types of dissipation-driven small-scale thermal convection in the mantle wedge are possible, viz. the 3D finger-like convective jets, raising to volcanic chain, and 2D transversal Karig vortices, aligned perpendicularly to subduction. These two types of convection are shown to be spatially separated due to the pressure and temperature dependence of mantle effective viscosity, the Karig vortices, if any of them formed, being located behind the volcanic arc [4]. There are contradictory judgments on the velocity of subduction of the Apulian lithospheric microplate under the Euro-Asian one, although the order of magnitude of the present-day subduction velocity ( $\sim 10$  mm $\times$ a<sup>-1</sup>) can apparently be regarded as established sufficiently reliably. The mountainous massif Dinarides locates parallel to the north-eastern shore of the Adriatic sea, and probably is of the thrust-and-fold nature. The 2D maximum of the heat flux anomaly of  $\sim 100$  mW $\times$ m<sup>-2</sup>

observed in the rear of the Dinarides massif in the Pannonia basin and the Vardar zone [10] can be assumed to owe its origin to the convective heat supply from the mantle wedge. Numerical modeling of the 2D convection, occurring in the mantle wedge in the form of the Karig vortices and presumably transporting heat upwards, allows to judge about the mean water content in the mantle wedge and to assume the mantle hydrocarbons to be transported to the Earth's surface by the upwelling convective flows. Numerical convection models accounting for the pressure-, temperature- and stress-dependence of viscosity fit best to observational data in the case of non-Newtonian rheology at the mantle water content of  $\sim (0.3 - 3) \times 10^1$  weight % for the velocity of subduction of  $\sim 10 \text{ mm} \times a^{-1}$  during the Middle Miocene. In [15] such rather a high water content (and even greater one, up to 3 weight %) can be observed in the mantle wedge in the mantle transition zone. The Middle Miocene subduction velocity of  $\sim 10 \text{ mm} \times a^{-1}$  during the formation of the Pannonia basin is of the order of the observed presently, or, can somewhat exceed it because of the gradual diminution of the velocity of convergence of African and Euro-Asian plates.

## II. THE COMPUTER THERMO-MECHANICAL MODEL

Thermo-mechanical model of the mantle wedge between the base of the overlying Euro-Asian plate and the upper surface of the Apulian lithospheric microplate subducting under the Euro-Asian one with a velocity  $V$  at an angle  $\beta$  is obtained for the infinite Prandtl number fluid as a solution of non-dimensional 2D hydrodynamic equations in the Boussinesq approximation

$$(\partial_{zz}^2 - \partial_{xx}^2) \times \eta \times (\partial_{zz}^2 - \partial_{xx}^2) \times \psi + 4 \times \partial_{xz}^2 \eta \times \partial_{xz}^2 \psi = Ra \times T_x - Ra^{(410)} \times \Gamma_x^{(410)} - Ra^{(660)} \times \Gamma_x^{(660)} \quad (1)$$

$$\partial_t T = \Delta T - (\psi_z \times T_x) + (\psi_x \times T_z) + (Di / Ra) \times (\tau_{ik}^2 / 2 \times \eta) + Q \quad (2)$$

For the stream-function  $\psi$  and temperature  $T$ . Here  $\eta$  is dynamic viscosity,  $\partial$  and indices denote partial derivatives with respect to coordinates  $x$  (horizontal),  $z$  (vertical) and time  $t$ ,  $\Delta$  is the Laplace operator,  $\Gamma^{(410)}$  and  $\Gamma^{(660)}$  are volume ratios of the heavy phase at the 410 km and 660 km phase boundaries, the velocity components  $V_x$  and  $V_z$  are expressed through  $\psi$  as

$$V_x = \psi_z, V_z = -\psi_x \quad (3)$$

while non-dimensional Rayleigh number  $Ra$ , phase numbers  $Ra^{(410)}$ ,  $Ra^{(660)}$  and dissipative number  $Di$  are

$$\begin{aligned} Ra &= [(a \times \rho \times g \times d^3 \times T_1) / (\eta_c \times \chi)] = 5.55 \times 10^8; \\ Ra^{(410)} &= [(\delta\rho^{(410)} \times g \times d^3) / (\eta_c \times \chi)] = 6.60 \times 10^8; \\ Ra^{(660)} &= [(\delta\rho^{(660)} \times g \times d^3) / (\eta_c \times \chi)] = 8.50 \times 10^8; \\ Di &= [(a \times g \times d) / c_p] = 0.165, \end{aligned} \quad (4)$$

where  $\alpha = 3 \times 10^{-5} \text{ K}^{-1}$  is the thermal expansion coefficient,  $\rho = 3.3 \text{ g} \times \text{cm}^{-3}$  is the density,  $g$  is gravity acceleration,  $c_p = 1.2 \times 10^3 \text{ J} \times \text{kg}^{-1} \times \text{K}^{-1}$  is specific heat capacity at constant pressure,  $T_1 = 1950 \text{ K}$  is the temperature at the base of mantle transition zone (MTZ) at depth 660 km regarded the lower boundary of the model domain,  $Q = 6.25 \times 10^{-4} \text{ mW} \times \text{m}^{-3}$  is the volumetric heat generation in the crust,  $\tau_{ik}$  is the viscous stress tensor,  $d = 660 \text{ km}$  is vertical dimension of the modeled domain,  $\eta_s = 10^{18} \text{ Pa} \times \text{s}$  is the viscosity scaling factor,  $\chi = 1 \text{ mm}^2 \times \text{s}^{-1}$  is thermal diffusivity,  $\delta\rho^{(410)} = 0.07\rho$  and  $\delta\rho^{(660)} = 0.09\rho$  are the density changes at the 410 km and 660 km phase boundaries respectively. In (1), (2) the scaling factors for time  $t$ , coordinates  $x$  and  $z$ , stresses  $\tau_{ik}$  and the stream-function  $\psi$  are  $(d^2 \times \chi^{-1})$ ,  $d$ ,  $(\eta_s \times \chi \times d^2)$  and  $\chi$  respectively. Assuming rheology be linear for the diffusion creep deformation mechanism dominating in the mantle at depths over  $\sim 200 \text{ km}$  [2], we accept the temperature- and lithostatic pressure  $p$  dependent viscosity as [15]:

$$\eta = (\mu / 2 \times A) \times (h / b^*)^m \times \{ \exp [ (E^* + p \times V^*) / (R \times T) ] \} \quad (5)$$

where for "wet" olivine  $A = 5.3 \times 10^{15} \text{ s}^{-1}$ ,  $m = 2.5$ , the grain size  $h = 10^{-1} - 10 \text{ mm}$ ,  $b^* = 5 \times 10^{-8} \text{ cm}$  is the Burgers vector [14],  $E^* = 240 \text{ kJ} \times \text{mol}^{-1}$  is activation energy,  $V^* = 5 \times 10^3 \text{ mm}^3 \times \text{mol}^{-1}$  is activation volume,  $\mu = 300 \text{ GPa}$  is the shear modulus normalizing factor,  $R$  is the gas constant. At the constants chosen and the grain size  $h = 1.6 \text{ mm}$ , non-dimensional viscosity also denoted  $\eta$  is

$$\eta = 5 \times 10^{-7} \times \exp \{ [14.8 + 6.72 \times (1 - z)] / T \} \quad (6)$$

where  $T$  is non-dimensional temperature, non-dimensional  $z$  normalized by  $d$  is pointing upwards from the MTZ base and  $x$  is pointing against subduction along the MTZ base. The aspect ratio of the model domain is 1:2.25 thus the subduction angle being  $\beta = 24^\circ$  if subduction is assumed to take place along the model domain diagonal. Non-dimensional subduction velocity

$V = 10 \text{ mm} \times a^{-1}$  normalized by  $(\chi \times d^1)$  equals  $V = 0.208 \times 10^3$ , i.e. non-dimensional velocity components of subducting Adriatic micro-plate are  $V_x = -0.190 \times 10^3$  and  $V_z = -0.085 \times 10^3$ .

To check as to how the estimate of velocity of subduction of the Adriatic micro-plate is sensitive to the accepted linear rheological law here we make extra computations for the non-Newtonian rheology, in which case the viscosity formulae (5)–(6) are rewritten as:

$$\eta = (1/2 \times A \times C_w^r \times \tau^{n-1}) \times (h/b^*)^m \times \{ \exp [ (E^* + p \times V^*) / (R \times T) ] \} \quad (7)$$

where according to [13] for “wet” olivine  $n = 3$ ,  $r = 1.2$ ,  $m = 0$ ,  $\tau = (\tau_{ik}^2)^{1/2}$ ,  $E^* = 480 \text{ kJ} \cdot \text{mol}^{-1}$ ,  $V^* = 11 \times 10^3 \text{ mm}^3 \times \text{mol}^{-1}$ ,  $A = 10^2 \text{ c}^{-1} \times (\text{MPa})^n$ ,  $C_w > 10^{-3}$  for “wet” olivine is the weight water concentration (in %). It should be noted the constants in (7) vary considerably in the papers referred to by [13] and heretofore we gave averaged values of constants. At  $C_w = 10^{-3}$  on accounting for

$$\tau_{ik}^2 = (4 \times \eta^2) \times [ (\psi_{zz} - \psi_{xx})^2 / 2 + 2 \times \psi_{xz}^2 ] \quad (8)$$

non-dimensional viscosity is

$$\eta = \{ 1.0 / [ (\psi_{zz} - \psi_{xx})^2 / 2 + 2 \times \psi_{xz}^2 ]^{1/3} \} \times \exp \{ [10.0 + 5.0 \times (1 - z)] / T \} \quad (9)$$

Following [13] we assume the phase functions  $\Gamma^{(l)}$  as

$$\Gamma^{(l)} = (1/2) \times \{ 1 - th [z - z^{(l)}(T)] / w^{(l)} \}; z^{(l)}(T) = z_o^{(l)} - \{ [\gamma^{(l)} \times (T - T_o^{(l)})] / (\rho \times g) \} \quad (10)$$

where the signs are changed as  $z$ -axis is pointing upwards,  $z^{(l)}(T)$  is the depth of the  $l$ -th phase transition ( $l = 410, 660$ ),  $z_o^{(l)}$  and  $T_o^{(l)}$  are the averaged depth and temperature of the  $l$ -th phase transition,  $\gamma^{(410)} = 3 \text{ MPa} \times \text{K}^{-1}$  and  $\gamma^{(660)} = -3 \text{ MPa} \times \text{K}^{-1}$  are the slopes of the phase equilibrium curves,  $w^{(l)}$  is the characteristic thickness of the  $l$ -th phase transition,  $T_o^{(410)} = 1800^\circ \text{ K}$ ,  $T_o^{(660)} = 1950^\circ \text{ K}$  are the mean phase transition temperatures. The heats of phase transitions are neglected in (2) as insignificant in the case of developed convection as in [13]. From (10) it follows

$$\Gamma_x^{(l)} = -(\gamma^{(l)} / 2 \times \rho \times g \times w^{(l)}) \times T_x \times ch^{-2} \{ [(z - z_o^{(l)} + \gamma^{(l)} \times (T - T_o^{(l)})) / (\rho \times g)] / w^{(l)} \} \quad (11)$$

Where from it is clear the phase transition with  $\gamma^{(l)} > 0$  facilitates convection (at  $l = 410$ ), while the phase transition with  $\gamma^{(l)} < 0$  hinders convection (at  $l = 660$ ). In non-dimensional form  $z_o^{(410)} = 0.38$ ,  $z_o^{(660)} = 0$ ,  $w^{(l)} = 0.05$ ,  $\gamma^{(410)} = 2.5 \times 10^9$ ,  $\gamma^{(660)} = -2.5 \times 10^9$ ,  $T_o^{(410)} = 0.92$ ,  $T_o^{(660)} = 1$  and in (1)

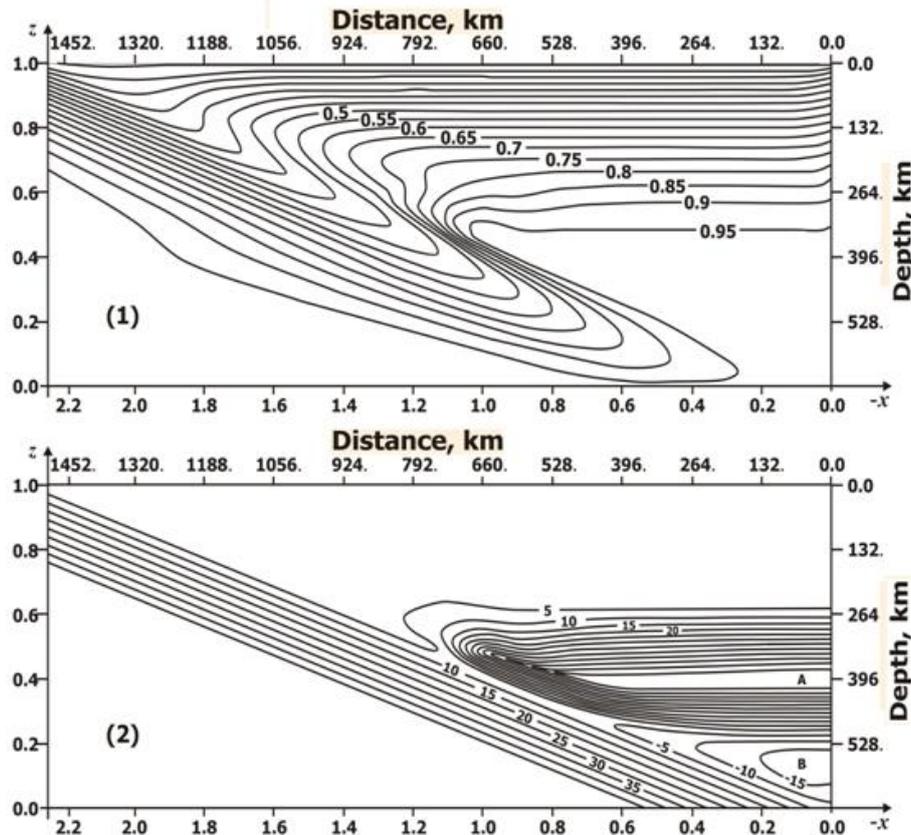
$$\Gamma_x^{(l)} = -(\delta \rho^{(\lambda)} \gamma^{(l)} / 2 \times \rho \times Ra^{(l)} \times w^{(l)}) \times T_x \times ch^{-2} \{ [z - z_o^{(l)} + \gamma^{(l)} (\delta \rho^{(\lambda)} / \rho \times Ra^{(l)}) \times (T - T_o^{(l)})] / w^{(l)} \} \quad (12)$$

Equations (1)–(2) are solved for the isothermal horizontal and vertical boundaries regarded no-slip impenetrable ones except for the “windows” for in- and outgoing subducting plate, where the plate velocity is specified. Vertical boundary distant from subduction zone is assumed penetrable at right angle; the latter boundary condition appears not too imposing in the case of very flat subduction.  $Q$  in (2) is non-zero in the continental and oceanic crust 40 and 7 km thick. Initial vertical boundaries temperature is calculated for the half-space cooling model for  $10^9$  yr and  $10^8$  yr for Euro-Asian (continental) plate and Apulian lithospheric microplate (paleoceanic plate) respectively. It is convenient to express dimensionless  $\tau_{ik}^2$  in (2) through the stream-function  $\psi$  as in (8):

$$\tau_{ik}^2 = (4 \times \eta^2) \times [ (\psi_{zz} - \psi_{xx})^2 / 2 + 2 \times \psi_{xz}^2 ]$$

### III. RESULTS AND DISCUSSION

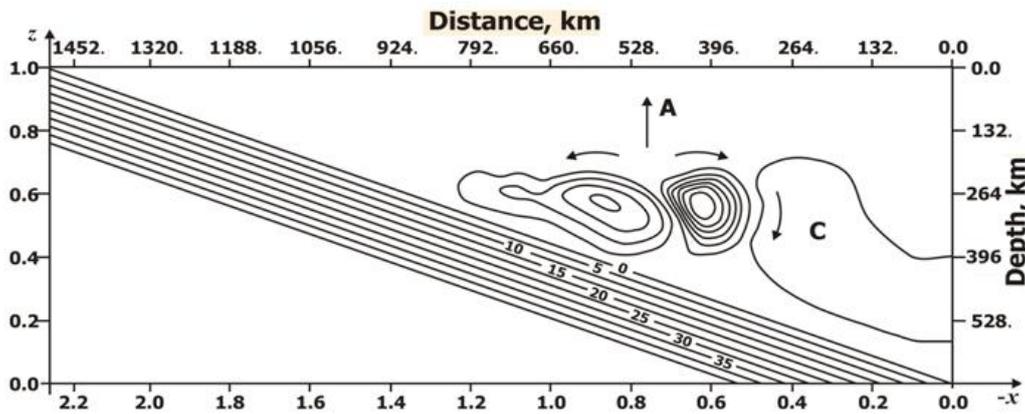
Assuming the heat flux maximum  $q$  is formed above the convective flow, upwelling towards the Pannonia basin and Vardar zone, and the convection cell dimension is equal to horizontal scale of the heat flux anomaly zone, the convection cell dimension can be estimated of  $\sim 300$  km. To more accurately compute the consistent model of small-scale convection in the mantle wedge between the overriding Euro-Asian plate and subducting Apulian lithospheric microplate it is necessary from the computational point of view first to specify in (1)–(2) vanishing non-dimensional numbers  $Ra \rightarrow 0$ ,  $Di = 0$ , i.e. to ignore convection and viscous dissipation. This approach is applied as convection with  $Ra$  and  $Di$  (4) passes through rather vigorous stages, and the time steps in integrating (1)–(2) become too small thus making it difficult to model the thermal structure of the plates. Solving (1)–(2) by the finite element method in space on the grid  $104 \times 104$  and the 3-rd order Runge-Kutta method in time one obtains for  $Ra \rightarrow 0$ ,  $Di = 0$  and  $V = 10$  mm a year non-dimensional quasi steady-state  $\psi$  and  $T$  shown in fig. 1, where the streamlines are depicted with the step 5 and the isotherms with an interval 0.05.



**FIGURE 1. Schematic cross section of the region of subduction of the Apulian lithospheric microplate under the Euro-Asian plate with no effects of viscous dissipation and convection taken into account. (1) – the quasi steady-state distribution of non-dimensional temperature and (2) – the quasi steady-state distribution of stream-function, the streamlines above the subducting slab correspond to the mantle wedge flows (“A” and “B”) induced by subduction.**

Subducting plate was considered rigid, while the viscosity at the zone of plates friction (at temperatures below  $1200^{\circ}\text{K}$ ) was reduced by 2 orders of magnitude as compared to (7). The latter viscosity reduction at the plates contact zone accounts for lubrication effected by deposits partially entrained by the subducting plate. Such a lubrication prevents the overriding Euro-Asian plate from gluing to the subducting one [9]. Fig. 1 shows the results of computation for the formulae (7) – (9) for non-Newtonian rheology case for the water content  $C_w = 3 \times 10^{-1}$  weight %. The velocity  $V = 10$  mm per year is chosen as resulting in the best fit of the model convective zone size to horizontal extent of the observed heat flux anomaly in Pannonia basin and the Vardar zone. The Apulian lithospheric microplate subducting with a given velocity  $V$  is considered rigid and is shown in Fig. 1(2) by the equidistant diagonal streamlines. The induced mantle wedge flow above the subducting plate is seen to occur in the form of two vortices A and B (located one above another), the latter 2 vortices being considerably compressed in the vertical direction and the upper one (with  $\psi > 0$ ) revolves clockwise while the lower one (with  $\psi < 0$ ) revolves counterclockwise. In Fig. 1(2) the upper induced flow “A” is seen to be firmly pressed to the subducting Apulian lithospheric microplate, the strain rate in the zone of contact of the opposite flows (i.e. flow “A” and subducting slab) being very high thus resulting in the viscosity (7) drop by several orders of magnitude. It should be noted that in the case of non-Newtonian rheology the greater the subduction angle the more extensive is this contact zone, in which the dissipative heat release mainly occurs. This may serve the reason why the Karig vortices (and the resulting back-arc spreading) are formed in the zones of comparatively steep subduction. The opposite flow “A” in Fig. 1(2) apparently is induced by the flow “B”, forced by subducting plate.

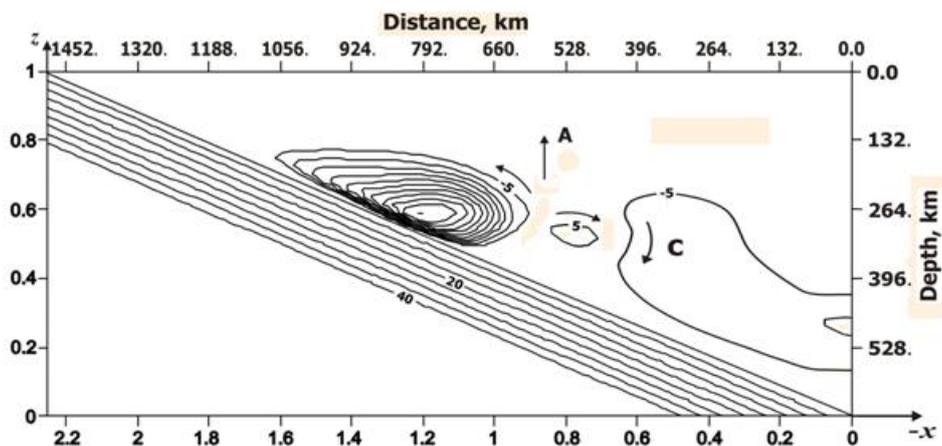
Assuming  $Ra = 5.55 \times 10^8$  and  $Di = 0.165$ , i.e. switching dissipation and convection on, taking into account the effects of phase transitions, from (1)–(2) the convection at  $C_w = 3 \times 10^{-1}$  weight % is found to destroy the induced mantle flows in the mantle wedge during the time interval  $\sim 0.6 \times 10^6$  (in dimensional form  $\sim 0.1$  Ma) and to assume the quasi steady-state form shown in Fig. 2, in which the streamlines in the convection vortices are depicted with the interval  $4 \times 10^4$ .



**FIGURE 2. Quasi steady-state non-dimensional stream-function distribution in the zone of subduction of the Apulian lithospheric microplate under the Euro-Asian plate with the effects of dissipative heating and convection taken into account for non-Newtonian rheology for the water content  $C_w=3\times 10^{-1}$  weight %. Parallel equidistant streamlines represent subducting Apulian lithospheric microplate. Arrow “A” shows possible direction of the upward convective transport of dissipative heat and mantle hydrocarbons to the Earth’s surface.**

These convective vortices are seen actually to correspond to a single convection cell aroused at subduction velocity  $V = 10 \text{ mm}\times a^{-1}$ . The latter convection cell dimension is of the order of  $\sim 300 \text{ km}$ , i.e. is very close to the observed horizontal extent of the heat flux anomaly observed in the Pannonia basin and Vardar zone. The velocity in convective vortices may exceed  $10 \text{ m}\times a^{-1}$  for the water content of  $3\times 10^{-1}$  weight %. The direction of a possible upward transport of mantle hydrocarbons and dissipative heat to the Earth’s surface is shown by the arrow “A”. It should be noted that in the case of Newtonian rheology the convection in the mantle wedge cannot be aroused at the velocity of subduction of  $10 \text{ mm}\times a^{-1}$  and subduction angle of  $25^\circ$ .

In Fig. 3 the quasi steady-state stream-function  $\psi$  is shown for the mantle water content of  $0.3\times 10^{-1}$  weight %, in which case the dissipation-driven convection is aroused in essentially a single vortex with a characteristic velocity of  $\sim 10 \text{ mm}\times a^{-1}$ .



**FIGURE 3. Quasi steady-state non-dimensional stream-function distribution in the zone of subduction of the Apulian lithospheric microplate under the Euro-Asian plate with the effects of dissipative heating and convection taken into account for non-Newtonian rheology for the water content  $C_w = 0.3\times 10^{-1}$  weight %. Parallel equidistant streamlines represent subducting Apulian lithospheric microplate. Arrow “A” shows possible direction of the upward convective transport of dissipative heat and mantle hydrocarbons to the Earth’s surface.**

This convective flow may serve a means of the upward mantle hydrocarbons and dissipative heat transport, which direction is shown in Fig. 3 by the arrow “A”. Such a convective flow may cause the back-arc spreading in the Pannonia basin and the Vardar zone. At the mantle water content  $C_w < 0.3\times 10^{-1}$  weight percent the dissipation-driven convection cannot be aroused

in the mantle wedge even in the case of the non-Newtonian rheology for subduction velocity of  $\sim 10 \text{ mm} \times a^{-1}$  and angle of  $25^\circ$ .

It is worth noting that in the case of Newtonian rheology the 2D transversal convective rolls in the mantle wedge, as in Fig. 2, can be formed only at sufficiently small angles of subduction. Thus, at  $\beta = 30^\circ$  the transversal convective rolls are not formed even at the velocity of subduction of  $100 \text{ mm} \times a^{-1}$  [5, 9]. In the case of the non-Newtonian rheology the transversal rolls (2D Karig vortices) can be aroused at greater subduction angles and sufficiently small subduction velocities owing to viscous friction in the zone of contact of the opposite induced flow ("A" in Fig. 1) and subducting slab. It should be noted that numerous thermo-mechanical mantle models in the zones of subduction (see, e.g. [8, 9] and the vast number of references there) showed convection in the form of transversal rolls never to occurred as the models with extremely small subduction angle and sufficiently great subduction velocity were not investigated.

#### IV. CONCLUSION

The size of the cell of 2D mantle wedge dissipation-driven convection in the case of the realistic non-Newtonian rheology equals  $\sim 300 \text{ km}$  at the subduction velocity  $10 \text{ mm} \times a^{-1}$ , in which case a single convection cell is aroused. This explains the formation and horizontal extent of the only 2D heat flux anomaly observed in the rear of the Dinarides. The water content sufficient for the 2D convection to be aroused is  $\sim 3 \times 10^{-1}$  weight %, or, alternatively, it is  $\sim 3 \times 10^{-2}$  weight %, but the 2D convection is aroused as a single Karig vortex. The velocity in convective vortices in the non-Newtonian rheology case is  $\sim 10 \text{ m}$  per year at the water content  $C_w \sim 3 \times 10^{-1}$  weight percent and  $\square 10 \text{ mm}$  per year at the water content  $C_w \sim 0.3 \times 10^{-1}$  weight percent in the mantle wedge. The upwelling convective flow may be sufficient to provide upward transport of mantle wedge hydrocarbons to the Earth's surface.

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